The readout thickness versus the measured thickness for a range of SFM and FFDM units

- 2 Ingrid H. R. Hauge^{a)}
- Oslo and Akershus University College of Applied Sciences, Faculty of Health Sciences,
- 4 Department of Radiography and Dental Technology, P. O. Box 4, St. Olavs plass, NO-0130 Oslo,
- Norway and Norwegian Radiation Protection Authority, P. O. Box 55, NO-1332 Østerås, Norway

6 Peter Hogg and Katy Szczepura

- Directorate of Radiography, University of Salford, Salford M6 6PU, United Kingdom
- 8 Paul Connolly
- 9 Integrated Radiological Services Ltd., Unit 188 Century Building, Tower Street, Brunswick Business Park,
- Liverpool L3 4BJ, United Kingdom
- 11 George McGill
- 12 The Christie NHS Foundation Trust, Wilmslow Road, Manchester M20 4BX, United Kingdom
- 13 Claire Mercer

17

19

20 21

24

25

26

28

29 30

31

45

47

- 14 Royal Bolton Hospital NHS Foundation Trust, Minerva Road, Farnworth, Bolton BL4 0JR, United Kingdom
- (Received 13 May 2011; revised 28 October 2011; accepted for publication 2 November 2011;
- published 0 0000)
 - **Purpose**: To establish a simple method to determine breast readout accuracy on mammography units.
 - **Methods**: A thickness measuring device (TMD) was used in conjunction with a breast phantom. This phantom had compression characteristics similar to human female breast tissue. The phantom was compressed, and the thickness was measured using TMD and mammography unit readout. Measurements were performed on a range of screen film mammography (SFM) and full-field digital mammography (FFDM) units (8 units in total; 6 different models/manufacturers) for two different sized paddles and two different compression forces (60 and 100 N).
 - **Results**: The difference between machine readout and TMD for the breast area, when applying 100 N compression force, for nonflexible paddles was largest for GE Senographe DMR+ (24 cm \times 30 cm paddle: +14.3%). For flexible paddles the largest difference occurred for Hologic Lorad Selenia (18 cm \times 24 cm paddle: +26.0%).
 - Conclusions: None of the units assessed were found to have perfect correlation between measured and readout thickness. TMD measures and thickness readouts were different for the duplicate units from two different models/manufacturers. © 2012 American Association of Physicists in Medicine. [DOI: 10.1118/1.3663579]

Key words: mammography, breast thickness, breast compression

2 I. INTRODUCTION

Accurate breast thickness estimation is required in order to 33 calculate the mean glandular dose (MGD). 1-3 Accuracy is 34 also required for density measurements (which can be used 35 for predicting breast cancer risk)⁴ and for estimation of breast tissue volume.^{5,6} Compression paddles may deform/ tilt during mammography and this can lead to differences 38 between the actual and readout (displayed by the mammography machine) thickness of the compressed breast. Under 40 realistic clinical imaging conditions (phantom-simulated) 42 this study aimed to conduct a comparative analysis of readout versus measured thicknesses over a range of mammog-43 44

Previous studies have highlighted inaccuracies with thickness readouts of mammography machines; some of these studies have also proposed methods which may provide a better estimate of the compressed breast thickness. ^{3,7–9} Diffey *et al.* ¹⁰ found a maximum variation of 21.1 mm in the

chest wall to nipple direction, while the paddle deformation in the lateral direction was found to be insignificant in comparison to the chest wall to nipple direction. Tyson *et al.*⁹ described a technique for measuring breast thickness by using optical stereoscopic photogrammetry. This method had a precision of >1 mm, and a measurement accuracy of >0.2 mm. The readout thickness for a number of different mammography systems was found to vary by as much as 15 mm when compressing the same breast or phantom.⁹ The value of the method developed by Tyson *et al.*⁹ was its accuracy; system use however is labor intensive, being highly dependent on room lighting and also on image quality. Mawdsley *et al.*⁷ developed functions that can estimate the compressed breast thickness based upon the machine readout thickness and compression force reported by the machine.

This study aimed to develop a simple, clinically adaptable and accurate method to measure the difference between the readout and measured thickness. Building on previous research there was particular interest in, the creation and

57

64

119

128

69 documentation of the physical breast phantom characteristics, particularly in relation to in-vivo female human breast 71 tissue. In order to investigate how the thickness readout and the thickness across the breast correlated, a breast thickness 72

measuring device (TMD) was constructed.

II. METHODS AND MATERIALS

81

82

83

85

86

87

90

91

92

93

94

95

97

99

100

101

102

103

104

105

106

75 The method comprised of three stages. First, a clinically realistic breast phantom and backing plate with the creation of a rigid torso was tested. Second, the TMD was designed 77 and tested. Finally, using the TMD, the breast phantom with its backing plate was used to assess several mammography 79 units/paddle combinations.

II.A. Design, creation, and validation of breast phantom

Three breast prostheses (small (220 cm³), medium (360 cm³), and large (700 cm³), Trulife, Sheffield, United Kingdom) were assessed for their compression characteristics. Each of the breast prostheses were adhered onto a semiflexible backing plate. The backing plate was mounted onto a rigid torso (Fig. 1) in order to simulate how a real breast will behave when it is compressed. The resistance to compression incurred by the torso changed the compressibility of the phantom to better simulate a real breast.

Six rubber balloons were glued onto the flexible backing plate. The balloons gave minor mobility similar to pectoral muscle and fascia. The phantom was glued onto the balloons and covered with layers of latex. The latex was painted across the surface of the phantom and along the edges, with fewer layers across the surface than around the edges. The backing plate was mounted onto a rigid torso (CIRS, Norfolk) using two ratchet straps, one above and one below the breast phantom. Before compressing the breast phantom, a lubricant was applied to the phantom. This allowed the compression paddle to slide smoothly over the breast surface when pressure was applied.

Using the three breast phantoms, mounted as described, compression (N)/thickness (mm) graphs were generated from 40 to 100 N stepping through 10 N values. For each phantom, the compressed breast thickness data were averaged and normalized (the data were normalized to 1 for 40 N



Fig. 1. Breast mounted to semiflexible background plate and rigid torso.

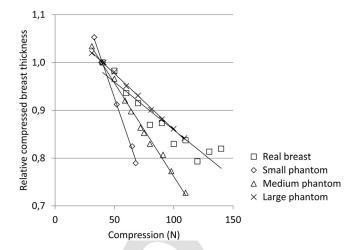


Fig. 2. Compressed breast thickness (mm) as a function of compression force (N) for real breasts and the three breast phantoms.

compression force). For comparison the normalized average 108 of 29 female human datasets were acquired (Fig. 2).

The 29 female datasets were acquired on a Hologic Lorad 110 Selenia, while the phantom data were collected from a GE 111 Senographe 800 T. The normalized compression curve of 112 the large prosthesis was compared with the normalized correlation curve of the real breast, and it was found that the 114 compression characteristics correlated well, with a correla-115 tion coefficient of 0.95. On this basis the large phantom 116 (700 cm³) was chosen as our breast phantom. 117

II.B. Compression paddle bend and distortion measuring device

The TMD was constructed of poly methyl methacrylate 120 (PMMA) (Fig. 3). TMD dimensions (depth: 17.1 cm, width: 121 36.0 cm, and height: 21.8 cm) were such that they would fit 122 the mammography machines/paddles that were to be 123 included in the study. Wooden rods, diameter approximately 124 5 mm, and of different lengths (10-25 cm) were used 125 (Fig. 3) to measure thickness. The top of the TMD had a matrix of 5 mm diameter holes drilled through it; the centers 127 were 20 mm apart.

II.C. How the study was conducted

The measurements were performed on different mam- 130 mography units from three different manufacturers [General 131



Fig. 3. Thickness measuring device (TMD) and rods.

PROOF COPY [11-560R1] 039112MPH

Hauge et al.: Readout thickness versus measured thickness

TABLE I. Mammographic units included in this study.

Location	Manufacturer/Model	SFM/FFDM	Compressed breast thickness accuracy (specified by manufacturer)	QC: maximum difference in measured and readout thickness ^b		Flexible/Nonflexib paddle	le Tilting/Nontilting
A	GE Senographe 800T	SFM	±10 mm	±0.4 cm	18 cm × 24 cm	Nonflexible	Nontilting
			$\pm 10 \text{ mm}$		$24 \text{ cm} \times 30 \text{ cm}$	Nonflexible	Nontilting
A	GE Senographe DMR+	SFM	$\pm 10 \text{ mm}$	+0.5 cm	$18 \text{ cm} \times 24 \text{ cm}$	Nonflexible	Nontilting
			$\pm 10 \text{ mm}$		$24 \text{ cm} \times 30 \text{ cm}$	Nonflexible	Nontilting
В	GE Senographe DMR+	SFM	$\pm 10 \text{ mm}$	+0.5 cm	$18 \text{ cm} \times 24 \text{ cm}$	Nonflexible	Nontilting
			$\pm 10 \text{ mm}$		$24 \text{ cm} \times 30 \text{ cm}$	Nonflexible	Nontilting
C	Siemens Mammomat Inspiration	FFDM	39–45 mm ^a	−0.1 cm	$18 \text{ cm} \times 24 \text{ cm}$	Nonflexible	Nontilting
					$24 \text{ cm} \times 30 \text{ cm}$	Nonflexible	Nontilting
В	GE Senographe Essential	FFDM	$\pm 10 \text{ mm}$	-0.3 cm	$19 \text{ cm} \times 23 \text{ cm}^{\text{d}}$	Nonflexible	Nontilting
			$\pm 10 \text{ mm}$		$19 \text{ cm} \times 23 \text{ cm}^{d}$	Flexible	Tilting
			$\pm 10 \text{ mm}$		$24 \text{ cm} \times 31 \text{ cm}$	Flexible	Tilting
D	Hologic Lorad Selenia	FFDM	± 0.5 cm	-0.1 cm	$18 \text{ cm} \times 24 \text{ cm}$	Flexible	Tilting
			± 0.5 cm		$24 \text{ cm} \times 30 \text{ cm}$	Flexible	Tilting
D	Hologic Selenia Dimensions	FFDM	± 0.5 cm	−0.1 cm	$18 \text{ cm} \times 24 \text{ cm}^{d}$	Flexible	Tilting
			± 0.5 cm		$24 \text{ cm} \times 29 \text{ cm}^{d}$	Flexible	Tilting
E	Hologic Lorad Selenia	FFDM	± 0.5 cm	−0.4 cm ^c	$18 \text{ cm} \times 24 \text{ cm}$	Flexible	Tilting
			±0.5 cm		$24 \text{ cm} \times 30 \text{ cm}$	Flexible	Tilting

^aThe thickness of a compressible phantom should be between 39 and 45 mm. The thickness of the compressible phantom (RMI 156, Gammex RMI, Middleton, WI) is 42 mm.

Electric (GE Medical Systems, Buc, France), Hologic Inc. (Bedford, MA) and Siemens (Siemens Healthcare, Erlangen, Germany)]. Both screen film mammography (SFM) and full-field digital mammography systems (FFDM) were included (Table I). This selection is representative of machines that were in clinical use at the time of the study. Two different paddle sizes, standard [approximately 18 cm \times 24 cm (18 \times 24)] and large [approximately 24 cm \times 30 cm (24 \times 30)] were used (Table I).

The TMD was placed on top of the table, with the long side (36.0 cm) parallel and along the edge of the chest side of the table top and centered left to right. The compression paddle was fastened such that it was located between the top and bottom plate of the TMD (Fig. 4), with the breast pros-



132

133

135

137

139

140

141

142 143

144



Fig. 4. How the measurements were conducted.

thesis resting on the bottom plate of the TMD. Two different 146 compression forces were applied when compressing the 147 breast prosthesis (60 and 100 N).

3

In order to estimate the compressed breast thickness, the 149 distance from the top of the TMD to the top of the compres- 150 sion paddle was measured across the whole area (Fig. 4). 151 The distance was measured by using a rod that was dropped 152 into the hole at the top of the TMD. A fingernail was used to 153 mark where the rod touched the top plate, the rod was then 154 removed and the length of the rod from the bottom (where it 155 touched the top of the compression paddle) up to the finger- 156 nail was measured using a ruler. This was repeated until the 157 height of the rod for all the holes that covered the compression paddle in question had been measured. Row 1 was 159 defined as the row parallel to the breast chest wall and clos- 160 est to the breast chest wall. Column 1 was defined as the col- 161 umn perpendicular to the breast chest wall and out to the left 162 side. Column 15 was then the last column on the right. A full 163 set of thickness measurements (105) took approximately 20 164 min to conduct.

Mawdsley *et al.*⁷ defined a reference point along the midline in the chest wall to nipple direction, 20 mm in from the chest wall side. They found that for most images the maximum height occurred at this reference point. We defined the same reference point in our study—hole in row 1, column 8 170 (located 2.5 cm from the breast chest wall side of the imaging table, and 18.0 cm from the short edge side).

^bIn the UK the compressed breast thickness accuracy is measured during quality control (QC) which is conducted every six months. This consists of measuring the compressed thickness for a PMMA phantom of known thickness. Difference in compressed breast thickness = Thickness of Perspex—Readout thickness. An under- and/or underestimation is considered equally faulty.

^cAll quality control measurements were conducted with a nonflexible paddle.

^dEven if Hologic Selenia Dimensions and GE Senographe Essential were a bit different in size than the others, they are referred to as $18 \text{ cm} \times 24 \text{ cm}$ (18×24) and $24 \text{ cm} \times 30 \text{ cm}$ (24×30) in the figures.

224

225

173

174

175

197

199

201

202

203

205

206

207

208

209

211

II.D. Calculation of breast thickness

The measurements performed to find the readout and measured thickness of the phantom is illustrated in Fig. 5.

The readout thickness (d) is given by the following 176 equation: 177

$$d = D - t \tag{1}$$

where D is the system readout thickness including the thickness 178 of the bottom plate. The thickness of the bottom plate (t) had to be subtracted from the total readout thickness (D) in order to 180 obtain the readout thickness for the phantom (d). The measured 181 thickness (M) of the object was calculated as follows:

$$M = H - t - p - 1 \tag{2}$$

where H is the total height of the TMD, p is the thickness of 183 the compression paddle, and l is the distance from the top of 184 the compression paddle to the top of the TMD. Using a ver- 185 nier caliper, the thickness of the compression paddles (p) 186 was measured to be 1.00 mm for Siemens Mammomat Inspi- 187 ration and 2.75 mm for all the other paddles in this study. 188 The area covering the compressed phantom (row 1 columns 189 3–13, row 2 columns 4–12, row 3 columns 6–10, and row 4 190 column 8) was defined as the breast area. The thickness for 191 the area covering the compressed breast phantom was measured (breast area), and the minimum, maximum and average 193 measured breast thickness for this area was compared to the 194 readout thickness, and the difference between them were 195 found, as follows-196

$$Percentage = \frac{(Average/min/max measured breast area) - Readout thickness}{Readout thickness}$$
(3)

A positive value implies that the measured thickness is larger than the readout thickness which suggests the machine underestimates thickness. A negative value implies that the measured thickness is smaller than the readout thickness, which suggests the machine overestimates the thickness. An over- or underestimation is considered equally faulty, and a difference close to zero is preferred.

II.E. TMD - precision and observer variability

Prior to commencing the study a precision and operator variability study was conducted. A wooden block (depth: 96 mm, width: 253 mm, and height: 55 mm) was placed inside the TMD device, centered in the middle and parallel to the long side of the TMD device. The thickness was measured three times by the person who would perform the thickness measurements. Average measured thickness was 55.5 mm, with a standard deviation of 0.4 mm across the whole area measured by the reader for all three measurements. The deviation in the measured thickness varied between -1 and 2142 mm (only one measurement varied with 2 mm) with an av- 215 erage of -0.04 ± 0.12 mm (95% confidence interval). Con- 216 cluding from this, this person would conduct the study with 217 good precision. However, in the study itself 15% of the 218 actual measurements were repeated on a blind sampling ba- 219 sis to minimize random error. The average difference 220 between the first measurement and the second measurement 221 (blind testing) was -0.17 ± 0.07 mm (95% confidence inter- 222 val). Concluding from this their precision and repeatability 223 was more than adequate for this study.

II.F. Quality control: checking the readout thickness

In the United Kingdom (the location for all the mammog- 226 raphy units in this study) the allowed difference between 227 readout and measured thickness is ±5 mm. 11 Each machine 228 was tested every six months (Table I); all units were operat- 229 ing within manufacturer specification.

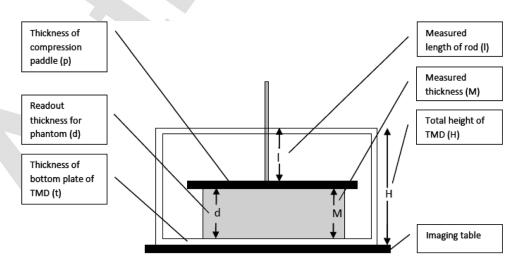


Fig. 5. Diagram to illustrate the measurements performed to calculate readout and measured thickness of the object.

Hauge et al.: Readout thickness versus measured thickness

II.G. Quality control: checking the compression force

Accuracy of compression force is assessed on traceably calibrated scales and noted to an accuracy of 5 N every 6 months by a medical physicist and monthly by radiographers. The readout compression force is checked for 40, 80, and 120 N and also at maximum compression force (200 N). The accuracy of the readout compared to the measured compression force was $\pm 10 \text{ N}$ (in accordance with IPEM 89 Ref. 11) for all the units.

III. RESULTS

231

232

234

235

236

237

239

240

241

243

245

247 248

251

252

257

Figures 6 and 7 illustrate a 3D representation of the difference between the measured thickness and the readout thickness for a nonflexible and flexible paddle across the whole measured area. Since the primary interest is the variation across the breast area, and the average percentage difference in compressed breast thickness, the minimum percentage difference in breast thickness and the percentage difference between readout and measured thickness for the reference point are shown in Fig. 8.

III.A. Difference between measured and readout thickness across paddle area

The smallest and largest difference between the measured and readout thickness of the compressed phantom across the whole measured area of the paddle is shown in Fig. 6 for the 18×24 flexible paddle (smallest difference: 12 mm and largest difference: 19 mm) and Fig. 7 for the 18×24 nonflexible paddle (smallest difference: 3 mm and largest difference: 7 mm). The average difference between the

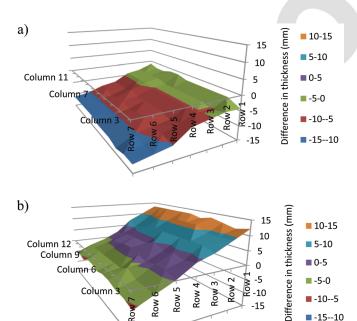


Fig. 6. Map of differences in thickness for the whole area for $18 \text{ cm} \times 24$ cm flexible compression paddle for (a) Hologic Selenia Dimensions, which had the smallest (12 mm) difference in thickness across the whole area and (b) Hologic Lorad Selenia, which had the largest (19 mm) difference in thickness across the whole area, when applying 100 N compression force.

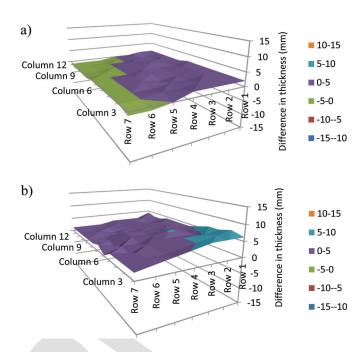


Fig. 7. Map of differences in thickness for the whole area for $18 \text{ cm} \times 24$ cm nonflexible compression paddle for (a) Siemens Mammomat Inspiration, which had the smallest (3 mm) difference between measured and readout thickness across the whole area and (b) GE Senographe 800 T, which had the largest (7 mm) difference in measured and readout thickness across the whole area, when applying 100 N compression force.

smallest and largest measured thickness across the whole 259 area was smaller for nonflexible paddles compared to flexi- 260 ble paddles (nonflexible/flexible 18×24 : 5.0/16.0 mm, 261 nonflexible/flexible 24×30 : 5.3/10.0 mm). Figure 7 illus- 262 trates that the compression paddle may be uneven in the left 263 to right direction.

The average, minimum, maximum percentage, and refer- 265 ence point percentage difference between measured com- 266 pressed breast thickness and the readout compressed breast 267 thickness for the breast area for the 18×24 paddle for 60 268 and 100 N applied compression force is shown in Fig. 8.

Figure 8 shows that there is a larger spread in the average 270 percentage difference for the flexible than for the nonflexible 271 compression paddle for both 60 N (range: -5.5%-6.8% 272 (nonflexible), -4.5%-9.0% (flexible)) and 100 N (range: 273 -8.0%-11.2% (nonflexible), -6.0%-26.0% (flexible), and 274 the difference is larger for 100 N than for 60 N applied com- 275 pression force. For the nonflexible paddles Siemens Mam- 276 momat Inspiration (60 N: 1.0%, 100 N: 2.6%) came closest 277 to 0% difference for the average percentage difference, and 278 for the flexible paddle Hologic Selenia Dimensions (60 N: 279 -1.5%) came closest to 0% difference when 60 N compression force was applied and GE Senographe Essential (100 N: 281 -3.1%) came closest to 0% difference when 100 N compression force was applied.

III.B. Variation in thickness across breast area

The average, minimum, and maximum differences 285 (measured in mm) for the compressed breast area is shown 286 in Table II.

283

284

Column 6

■ 0-5

-10--5

-15--10

-5 -10

289

290

291

292

293

295

297

299

300

301

302

303

304

305

306

307

308

309

310

311

313

315

Hauge et al.: Readout thickness versus measured thickness

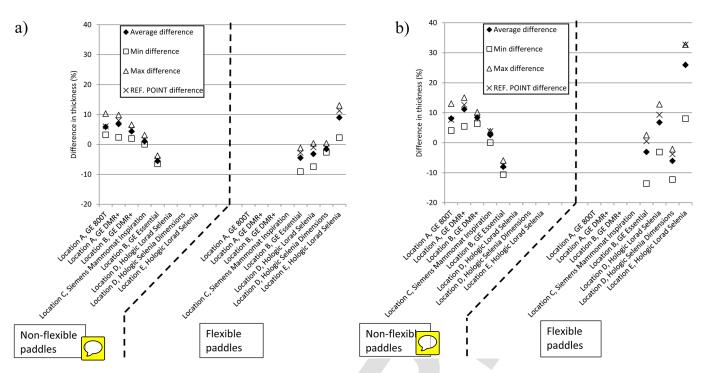


Fig. 8. The percentage difference between measured thickness and readout thickness for the breast area for 18 cm × 24 cm nonflexible and flexible compression paddle for (a) 60 N and (b) 100 N applied compression force.

The difference between machine readout and measured thickness for nonflexible paddles for the breast area, applying 100 N compression force was smallest for the Siemens Mammomat Inspiration (18 \times 24 paddle: +2.6% (p < 0.01), 24 \times 30 paddle: +0.7% (p = 0.05)) and largest for GE Senographe DMR+ $(18 \times 24 \text{ paddle (location A): } +11.2\% \text{ } (p < 0.01),$ 24×30 paddle (location B): +14.3% (p < 0.01)). For the 18×24 flexible paddle, and with an applied compression force of 100 N, the smallest difference between machine readout and measured thickness for the breast area occurred for GE Senographe Essential [-3.1% (p < 0.01)], and the largest for a Hologic Lorad Selenia [26.0% (p < 0.01)]. For the 24 \times 30 flexible paddle, and with an applied compression force of 100 N, the smallest difference between machine readout and measured thickness for the breast area occurred for a Hologic Lorad Selenia [3.0% (p < 0.01)] and the largest difference occurred for the other Hologic Selenia Dimensions [-8.9% (p < 0.01)].

The average differences for both paddles, both compression forces (60 and 100 N) and all modalities in this study were +2.6% (60 N: +1.3%, 100 N: +2.8%).

In this study, two Hologic Lorad Selenia and two GE Essential DMR+ units were included. When comparing the results for the two units of equal manufacturer and model, it was found that the average difference between the readout thickness and the measured thickness for the breast area is different for the two units [GE DMR+: 11.2 vs 8.4% (18×24) , 0.7 vs 14.3% (24×30) , Hologic Lorad Selenia: 6.8 vs 26.0% (18 \times 24), 3.0 vs 8.3% (24 \times 30)].

III.C. Change in measured compressed breast thickness when increasing the compression force

When increasing the compression force from 60 to 100 N an 18% decrease in measured compressed breast thickness was observed for the breast area $(18 \times 24: 17.8 \pm 1.4\%, 320)$ 24×30 : 17.7 $\pm 5.4\%$) when using nonflexible paddles. When 321 using flexible paddles a larger decrease in measured com- 322 pressed breast thickness can be observed for the 18×24 pad- 323 dles $(18.6 \pm 2.6\%)$ versus the 24×30 paddles $(17.1 \pm 1.9\%)$. 324

6

331

345

346

III.D. Reference point

The average difference for both compression forces, both 326 paddles (nonflexible/flexible) and both paddle sizes between 327 the measured thickness for the average breast area and the 328 measured thickness for the reference point is -0.7 ± 0.2 mm ³²⁹ (in percentage: $-1.4 \pm 0.5\%$). 330

IV. DISCUSSION

For all machine and paddle combinations the readout breast 332 thickness was different to; reference point thickness, average 333 thickness, minimum thickness, or maximum thickness. This 334 resulted in the measured thickness being over-estimated and 335 also under-estimated. The difference was more marked at 100 336 N compared with 60 N, suggesting that as force increases the 337 error in thickness readout also increases. At 100 N and 18×24 paddle, only 2 (Location B GE Essential/18 × 24 flexible; 339 Location C, Siemens Mammomat Inspiration/18 \times 24/24 \times 30 340 nonflexible) out of 9 machines (22%) gave reference point and 341 average values for the breast area that were within $\pm 5\%$ of the 342 readout thickness. Flexible paddles had greater departure from 343 measured thickness when compared with nonflexible paddles.

IV.A. Quality control and tolerance data supplied by manufacturers

The results for the average difference in compressed 347 breast thickness for the breast area was compared to the 348

PROOF COPY [11-560R1] 039112MPH

Hauge et al.: Readout thickness versus measured thickness

Table II. Average, minimum and maximum difference in thickness (mm) for the breast area for the compression forces 60 and 100 N for the different mammography units included in this study.

	Compression force 60 N				Compression force 100 N			
	Average difference mm (%) ^a	Min difference mm (%) ^b	Max difference mm (%) ^c	Ref. point difference mm (%) ^d	Average difference mm (%) ^a	Min difference mm (%) ^b	Max difference mm (%) ^c	Ref. point difference mm (%) ^d
Nonflexible paddle, 18×24								
Location A, GE 800T	4.1 (5.9)	2.3 (3.2)	7.3 (10.3)	4.3 (6.0)	4.5 (8.1)	2.3 (4.1)	7.3 (10.3)	4.3 (7.7)
Location A, GE DMR+	3.6 (6.8)	1.3 (2.3)	5.3 (9.8)	4.3 (7.9)	4.6 (11.2)	2.3 (5.4)	6.3 (15.1)	5.3 (12.7)
Location B, GE DMR+	2.8 (4.3)	1.3 (1.9)	4.3 (6.6)	3.3 (5.0)	4.3 (8.4)	3.3 (6.3)	5.3 (10.2)	4.3 (8.3)
Location B, GE Essential	-2.8(-4.5)	-0.8(-1.2)	-5.8(-9.1)	-1.8(-2.8)	-1.5(-3.1)	1.3 (2.5)	$-14.8 \; (-13.6)$	0.3 (0.5)
Location C, Siemens Mammomat Inspiration	0.7 (1.0)	0.0(0.0)	2.0 (3.1)	1.0 (1.6)	1.3 (2.6)	0.0(0.0)	2.0 (3.8)	2.0 (3.8)
Nonflexible paddle, 24×30								
Location A, GE 800T	2.8 (5.0)	2.3 (4.1)	4.3 (7.7)	3.3 (5.9)	3.4 (7.7)	1.3 (2.8)	4.3 (9.6)	3.3 (7.3)
Location A, GE DMR+	3.9 (7.4)	3.3 (6.1)	5.3 (9.8)	4.3 (7.9)	0.3 (0.7)	-0.8(-1.8)	1.3 (2.9)	1.3 (2.9)
Location B, GE DMR+	4.6 (9.7)	2.3 (4.7)	7.3 (15.3)	5.3 (11.1)	5.6 (14.3)	3.3 (8.2)	7.3 (18.4)	6.3 (15.7)
Location C, Siemens Mammomat Inspiration	0.1 (0.1)	-1.0(-1.6)	2.0 (3.3)	0.0 (0.0)	0.3 (0.7)	-1.0(-1.9)	2.0 (3.8)	1.0 (1.9)
Flexible paddle, 18×24								
Location B, GE Essential	-2.8 (-4.5)	-0.8(-1.2)	-5.8 (-9.1)	-1.8(-2.8)	-1.5 (-3.1)	1.3 (2.5)	-6.8 (-13.6)	0.3 (0.5)
Location D, Hologic Lorad Selenia	-2.4(-3.2)	0.3 (0.3)	-5.8(-7.4)	-0.8(-1.0)	3.8 (6.8)	-1.8(-3.1)	7.3 (12.8)	5.3 (9.3)
Location D, Hologic Selenia Dimensions	-1.0(-1.5)	0.3 (0.4)	-1.8(-2.6)	-0.8(-1.1)	-3.6(-6.0)	-1.3(-2.1)	-7.3(-12.3)	-2.3(-3.8)
Location E, Hologic Lorad Selenia	5.0 (9.0)	1.3 (2.3)	7.3 (13.1)	6.3 (11.3)	10.5 (26.0)	3.3 (8.0)	13.3 (32.7)	13.3 (32.7)
Flexible paddle, 24×30								
Location B, GE Essential	-2.9(-4.4)	-1.8(-2.7)	-3.8(-5.8)	-2.8(-4.2)	-3.8(-7.0)	-2.8(-5.1)	-4.8(-8.7)	-2.8(-5.1)
Location D, Hologic Lorad Selenia	-4.1 (-4.9)	-2.8(-3.3)	-5.8(-6.8)	-3.8(-4.4)	2.0 (3.0)	-1.8(-2.6)	4.3 (6.4)	3.3 (4.9)
Location D, Hologic Selenia Dimensions	-4.8(-8.9)	-1.8(-2.9)	-2.8 (-4.5)	-1.8(-2.9)	-4.8(-8.9)	-2.3 (-4.2)	-8.3(-15.3)	-2.3 (-4.2)
Location E, Hologic Lorad Selenia	0.2 (0.3)	1.3 (1.9)	-1.8(-2.6)	1.3 (1.9)	4.5 (8.3)	1.3 (2.3)	7.3 (13.3)	6.3 (11.5)

^aAverage difference: average difference between measured and readout thickness across the area defined as the breast area.

maximum difference in measured thickness (for phantom of known thickness) and readout thickness from the annual quality control. Only two units (GE Senographe DMR+ (Location A) and GE Senographe Essential) of the eight units (25%) were found to have an average difference between measured and readout thickness within the maximum difference found at the annual quality control. For the Hologic Lorad Selenia at Location D the average difference was larger than the difference between measured and readout thickness from the quality control for both paddles and both compression forces. For the other units (GE Senographe 800T, GE Senographe DMR+ (Location B), Siemens Mammomat Inspiration, Hologic Selenia Dimensions and Hologic Lorad Selenia (Location E)) discrepancies were found for 18×24 and/or 24×30 paddle and/or for both compression forces (60 and 100 N). The results in this study show that the test performed annually by the medical physicist might not be adequate to reveal discrepancies between the measured and the readout thickness.

349

351 352

353

354

355

356

357

358

360

361

362

363

364

365

366

367

369

370

371

372

Our measurements for the compressed breast thickness were compared to the tolerance data stated in the operator manuals supplied by the different manufacturers. For GE Senographe 800T and GE Senographe DMR+ our results were within the tolerance limits of ± 10 mm stated in the operator manuals. Hologic Lorad Selenia user manual states

that compression thickness accuracy should be ± 0.5 cm for 374 thicknesses between 0.5 and 15 cm. This was found to be 375 true for one of the Hologic Lorad Selenia units (difference in 376 measured and readout thickness for average breast area: 3.8 377 mm), but not for the other unit [difference in measured and 378 readout thickness for average breast area: 10.5 mm 379 (18×24)], when the 18×24 paddle was used and 100 N 380 compression force was applied. For GE Senographe Essen- 381 tial the difference between the measured and readout thick- 382 ness for the breast area was within the tolerance limit (± 10 383 mm). Had the tolerance limit been ± 5 mm, in other words 384 the same as for Hologic Lorad Selenia/Hologic Selenia 385 Dimensions, the results for the minimum difference between 386 measured and readout thickness for the 18×24 paddles 387 (nonflexible and flexible), when 100 N compression force 388 was applied, would have also been within the limits.

7

To calibrate the readout thickness Siemens uses a 42 mm 390 phantom and compresses the object using a 70 N compression force. The readout thickness should read between 39 392 and 45 mm. If not a recalibration is performed.

A calibration of the Hologic Lorad Selenia is performed 394 by compressing a 5 cm thick phantom (BR-12, CIRS, Nor-395 folk, VA). A compression force of 133.5 N is applied, and 396 then the compression thickness is calibrated for the installed 397 paddle/receptor combination. 398

^bMin difference: minimum difference between measured and readout thickness across the area defined as the breast area.

^cMax difference: maximum difference between measured and readout thickness across the area defined as the breast area.

^dRef. point difference: difference between measured and readout thickness for the hole defined as the reference point (row 1, column 8).

400

401

402

403

405

407

408

409

410

411

412

413

414

415

416

417

419

420

421

422

423

424

426

427

428

429

430

431

432

433

435

436

437

439

440

441

442

446

448

Hauge et al.: Readout thickness versus measured thickness

For Hologic Selenia Dimensions most of the calibration is done automatically. A 2 and 8 cm thick phantom (BR-12) is compressed by applying 133.5 N compression force, and the machine will then register the thickness of the phantom. For the "FAST" paddle (the flexible paddle) the same approach is taken, but without any compression. The paddle is just lowered until it touches the phantom, and the machine is told that this is 2 or 8 cm. The fact that a rigid phantom is used for this test is probably not optimal, because a tilt will probably occur. Maybe one needs to rethink how the thickness is measured, or maybe a different approach to how the paddle is constructed needs to be addressed.

GE also has routines for the calibration of the thickness, but the calibration routines are propriety.

IV.B. Reference point

The difference between readout and measured thickness for the reference point and the average breast area values are similar $[-0.7 \pm 0.2 \text{ mm} \text{ (in percentage: } -1.4 \pm 0.5\%)], \text{ sug-}$ gesting that a simplistic one-point of sample could be used for accurate estimation of average breast thickness. This approach would involve sampling only at the reference point, which would mean that the measuring time for the thickness would decrease drastically (from a maximum of 105 measurements down to one). We found that there is a large variation in the chest wall to nipple direction, and a smaller lateral variation, in accordance with Diffey et al. 10 A better estimate would therefore be to measure the thickness for the points/holes outlining the breast area; in this way, a better average for the compressed breast thickness could be measured.

Where Diffey et al. 10 found for real breasts an underestimation of thickness of as much as 21.2 mm in the chest to nipple direction, our results show a maximum underestimation of 13 mm for a Hologic Lorad Selenia mammography machine, and a maximum overestimation of 8 mm for a Hologic Selenia Dimensions mammography machine. If one takes into consideration this under-/overestimation of thickness only (and not the fact that a change in the thickness might also have implications for the choice of target/filtercombination and kV), the MGD can be estimated. For a Hologic Lorad Selenia, for instance, an underestimation of 13 mm would imply a smaller estimated MGD of 17% for a thin breast (readout thickness 35 mm) and 9% for a thick breast (readout thickness 80 mm). An underestimation of thickness will in general imply that the MGD originally estimated is too large, and thus overestimate the MGD and the risk. For a Hologic Lorad Dimensions an overestimation of 8 mm would imply a larger estimated MGD of 20% for a thin breast (readout thickness 31 mm) and 6% for a thick breast (readout thickness 79 mm). An overestimation of thickness will in general imply that the MGD originally estimated is too small, and thus underestimate the MGD and the risk.

IV.C. Correction factor 450

Varying paddle/machine combinations give different 451 error levels between readout thickness and measured thickness. Correction factors may be applied, in order to obtain higher accuracy clinically. The correction factor can be 454 found by dividing the measured thickness with the readout 455 thickness for different manufacturers/models, different pad- 456 dle sizes (in this study: 18×24 and 24×30) and different 457 breast compression forces (in this study: 60 and 100 N).

8

459

488

489

504

IV.D. Study limitations

Preservation of breast phantom integrity limited our 460 experiment to a maximum pressure force of 100 N. We pro- 461 pose that a more resilient breast phantom should be used 462 across a broader range of clinically representative force values 463 (e.g., 60 N stepping 10 to 150 N). This would provide a better 464 understanding on how bend and distortion may vary across 465 the higher end of the normal clinical pressure range. In this 466 study the effect of different breast volumes or breast densities 467 was not considered; extending these variables might be con- 468 sidered, as bend and distortion may be affected by them.

A further limitation in this study is the fact that a different 470 readout thickness was achieved every time the measure- 471 ments were repeated. When compressing the phantom, dif- 472 ferent thicknesses were achieved every time; as such the 473 results are not reproducible. Positioning error was reduced 474 by trying to position the phantom approximately in the mid-475 dle of the compression paddle (along midline), but the com- 476 pressed thickness still altered.

Tyson et al. devised a method for determining the compressed breast thickness that had a thickness determination 479 accuracy of better than 1 mm, and a measurement accuracy 480 of better than 0.2 mm. The method described here will lead 481 to a larger inaccuracy than the method described by Tyson 482 et al. Tyson et al. state that a mean accuracy of better than 483 1 mm is required to make good estimates for the volumetric 484 breast density. It was not possible with the device used in 485 this study to obtain such a precision, but as for use in a busy 486 clinically environment the TMD can be used to determine 487 the difference in measured and readout thickness.

IV.E. Clinically adaptable method

In theory this method can be applied for real breasts in a 490 clinic to measure the real compressed breast thickness for the 491 breast. The breast must be placed inside the TMD, in the 492 same fashion as the phantom, compression must be applied 493 and the compressed breast thickness must be measured. 494 Because of the time span (20 min) for measuring the com- 495 pressed breast thickness in this study, it will probably be nec- 496 essary to limit the number of measurements performed to 497 only one point (e.g., the reference point). The breast must 498 then be recompressed (applying the same compression force) 499 in order to obtain the actual image. This last step will prob- 500 ably be difficult to accomplish, since it has been shown to be 501 difficult to obtain the same thickness applying the same com- 502 pression force when compressing an object similar to a breast. 503

V. CONCLUSION

The difference in the readout thickness and the measured 505 thickness varies between units for the same model and 506

J_ID: MPH DOI: 10.1118/1.3663579 Date: 10-December-11 Stage: Page: 9 Total Pages: 9

PROOF COPY [11-560R1] 039112MPH

9 Hauge et al.: Readout thickness versus measured thickness

07	between manufacturers. Individual correction factors for
808	breast thickness may need to be established for each depend
609	ent on paddle selection and compression force applied. Any
10	corrections to compressed breast thickness need therefore to
11	be performed for the unit in question, and one cannot assume
12	that the correction in compressed breast thickness applies to
13	all mammography machines of the same model

ACKNOWLEDGMENTS

516

517518

The authors would like to thank Steve Curtis from the Guitar Repair Workshop (Manchester, United Kingdom) for making the TMD.

19	^{a)} Electronic mail: ingrid-helen.ryste-hauge@hioa.no
20	¹ D. R. Dance, "Monte Carlo calculation of conversion factors for the estima
21	tion of mean glandular breast dose," Phys. Med. Biol. 35, 1211–1219 (1990)
22	² D. R. Dance, C. L. Skinner, K. C. Young, J. R. Beckett, and C. J. Kotre
23	"Additional factors for the estimation of mean glandular breast dose usin
24	the UK mammography dosimetry protocol," Phys. Med. Biol. 45
25	3225–3240 (2000).

³R. P. Highnam, J. M. Brady and B. J. Shepstone, "Estimation of compressed breast thickness during mammography," Br. J. Radiol. 71, 646–653 (1998).

⁴ N. F. Boyd, H. Guo, L. J. Martin, L. Sun, J. Stone, E. Fishell, R. A. Jong,	529
G. Hislop, A. Chiarelli, S. Minkin, and M. J. Yaffe, "Mammographic den-	530
sity and the risk and detection of breast cancer," N. Engl. J. Med. 356,	531
227–236 (2007).	532
⁵ J. J. Heine, K. Cao, and J. A. Thomas, "Effective radiation attenuation cal-	533
ibration for breast density: compression thickness influences and	534
correction," Biomed. Eng. Online 9, 73 (2010).	535
⁶ N. Boyd, L. Martin, A. Gunasekara, O. Melnichouk, G. Maudsley, C.	536
Peressotti, M. Yaffe, and S. Minkin, "Mammographic density and breast	537
cancer risk: evaluation of a novel method of measuring breast tissue vol-	538
umes," Cancer Epidemiol. Biomarkers Prev. 18, 1754–1762 (2009).	539
⁷ G. E. Mawdsley, A. H. Tyson, C. L. Peressotti, R. A. Jong, and M. J.	540
Yaffe, "Accurate estimation of compressed breast thickness in	541
mammography," Med. Phys. 36, 577–586 (2009).	542
⁸ A. Burch and J. Law, "A method for estimating compressed breast thick-	543
ness during mammography," Br. J. Radiol. 68, 394–399 (1995).	544
⁹ A. H. Tyson, G. E. Mawdsley, and M. J. Yaffe, "Measurement of com-	545
pressed breast thickness by optical stereoscopic photogrammetry," Med.	546
Phys. 36 , 569–576 (2009).	547
¹⁰ J. Diffey, A. Hufton, C. Beeston, J. Smith, T. Marchant, and S. Astley,	548
"Quantifying breast thickness for density measurement," in Digital Mam-	549
mography, 9th International Workshop, IWDM 2008, Tucson, AZ, edited by	550
E. A. Krupinski (Springer-Verlag, Berlin/Heidelberg, 2008), pp. 651–658.	551
¹¹ A. C. Moore, D. R. Dance, D. S. Evans, C. P. Lawinski, E. M. Pitcher, A.	552
Rust, and K. C. Young, IPEM Report 89: Commissioning and Routine	553
Testing of Mammographic X-Ray Systems (Institute of Physics and Engi-	554
neering in Medicine, 2005).	555

9

